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|-----------------|--------------|---------------|----------------------------|
| Company Name | IIT Bombay | Project Title | Tension Member |
| Group/Team Name | Osdag | Subtitle | Bolted to End Gusset |
| Designer | Engineer#1 | Job Number | 2.1.3 |
| Date | 04 /02 /2021 | Client | Mr. Yogesh D Pisal, Mumbai |

1 Input Parameters

| | |
|--|--|
| Module | Tension Member Design - Bolted to End Gusset |
| Axial (kN)* | 180.0 |
| Length (mm) * | 2500.0 |
| Section Profile* | Star Angles |
| Section Size* | Ref List of Input Section |
| Section Material | E 165 (Fe 290) |
| Ultimate Strength, F_u (MPa) | 410 |
| Yield Strength, F_y (MPa) | 250 |
| Bolt Details - Input and Design Preference | |
| Diameter (mm) | [16, 20] |
| Property Class | [5.6, 5.8, 6.8] |
| Type | Bearing Bolt |
| Hole Type | Standard |
| Detailing - Design Preference | |
| Edge Preparation Method | Sheared or hand flame cut |
| Are the Members Exposed to Corrosive Influences? | False |
| Plate Details - Input and Design Preference | |
| Thickness (mm) | [10, 12, 14] |
| Material | E 250 (Fe 410 W)A |



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1.1 List of Input Section

| | |
|---------------|--|
| Section Size* | '20 x 20 x 3', '20 x 20 x 4', '25 x 25 x 3', '25 x 25 x 4', '25 x 25 x 5', '30 x 30 x 3', '30 x 30 x 4', '30 x 30 x 5', '35 x 35 x 3', '35 x 35 x 4', '35 x 35 x 5', '35 x 35 x 6', '40 x 40 x 3', '40 x 40 x 4', '40 x 40 x 5', '40 x 40 x 6', '45 x 45 x 3', '45 x 45 x 4', '45 x 45 x 5', '45 x 45 x 6', '50 x 50 x 3', '50 x 50 x 4', '50 x 50 x 5', '50 x 50 x 6', '55 x 55 x 4', '55 x 55 x 5', '55 x 55 x 6', '55 x 55 x 8', '60 x 60 x 4', '60 x 60 x 5', '60 x 60 x 6', '60 x 60 x 8', '65 x 65 x 4', '65 x 65 x 5', '65 x 65 x 6', '65 x 65 x 8', '70 x 70 x 5', '70 x 70 x 6', '70 x 70 x 8', '70 x 70 x 10', '75 x 75 x 5', '75 x 75 x 6', '75 x 75 x 8', '75 x 75 x 10', '80 x 80 x 6', '80 x 80 x 8', '80 x 80 x 10', '80 x 80 x 12', '90 x 90 x 6', '90 x 90 x 8', '90 x 90 x 10', '90 x 90 x 12', '100 x 100 x 6', '100 x 100 x 8', '100 x 100 x 10', '100 x 100 x 12', '110 x 110 x 8', '110 x 110 x 10', '110 x 110 x 12', '110 x 110 x 16', '130 x 130 x 8', '130 x 130 x 10', '130 x 130 x 12', '130 x 130 x 16', '150 x 150 x 10', '150 x 150 x 12', '150 x 150 x 16', '150 x 150 x 20', '200 x 200 x 12', '200 x 200 x 16', '200 x 200 x 20', '200 x 200 x 25', '50 x 50 x 7', '50 x 50 x 8', '55 x 55 x 10', '60 x 60 x 10', '65 x 65 x 10', '70 x 70 x 7', '100 x 100 x 7', '100 x 100 x 15', '120 x 120 x 8', '120 x 120 x 10', '120 x 120 x 12', '120 x 120 x 15', '130 x 130 x 9', '150 x 150 x 15', '150 x 150 x 18', '180 x 180 x 15', '180 x 180 x 18', '180 x 180 x 20', '200 x 200 x 24', '30 x 20 x 3', '30 x 20 x 4', '30 x 20 x 5', '40 x 25 x 3', '40 x 25 x 4', '40 x 25 x 5', '40 x 25 x 6', '45 x 30 x 3', '45 x 30 x 4', '45 x 30 x 5', '45 x 30 x 6', '50 x 30 x 3', '50 x 30 x 4', '50 x 30 x 5', '50 x 30 x 6', '60 x 40 x 5', '60 x 40 x 6', '60 x 40 x 8', '65 x 45 x 5', '65 x 45 x 6', '65 x 45 x 8', '70 x 45 x 5', '70 x 45 x 6', '70 x 45 x 8', '70 x 45 x 10', '75 x 50 x 5', '75 x 50 x 6', '75 x 50 x 8', '75 x 50 x 10', '80 x 50 x 5', '80 x 50 x 6', '80 x 50 x 8', '80 x 50 x 10', '90 x 60 x 6', '90 x 60 x 8', '90 x 60 x 10', '90 x 60 x 12', '100 x 65 x 6', '100 x 65 x 8', '100 x 65 x 10', '100 x 75 x 6', '100 x 75 x 8', '100 x 75 x 10', '100 x 75 x 12', '125 x 75 x 6', '125 x 75 x 8', '125 x 75 x 10', '125 x 95 x 6', '125 x 95 x 8', '125 x 95 x 10', '125 x 95 x 12', '150 x 115 x 8', '150 x 115 x 10', '150 x 115 x 12', '150 x 115 x 16', '200 x 100 x 10', '200 x 100 x 12', '200 x 100 x 16', '200 x 150 x 10', '200 x 150 x 12', '200 x 150 x 16', '200 x 150 x 20', '40 x 20 x 3', '40 x 20 x 4', '40 x 20 x 5', '60 x 30 x 5', '60 x 30 x 6', '60 x 40 x 7', '65 x 50 x 5', '65 x 50 x 6', '65 x 50 x 7', '65 x 50 x 8', '70 x 50 x 5', '70 x 50 x 6', '70 x 50 x 7', '70 x 50 x 8', '75 x 50 x 7', '80 x 40 x 5', '80 x 40 x 6', '80 x 40 x 7', '80 x 40 x 8', '80 x 60 x 6', '80 x 60 x 7', '80 x 60 x 8', '90 x 65 x 6', '90 x 65 x 7', '90 x 65 x 8', '90 x 65 x 10', '100 x 50 x 6', '100 x 50 x 7', '100 x 50 x 8', '100 x 50 x 10', '100 x 65 x 7', '120 x 80 x 8', '120 x 80 x 10', '120 x 80 x 12', '125 x 75 x 12', '135 x 65 x 8', '135 x 65 x 10', '135 x 65 x 12', '150 x 75 x 9', '150 x 75 x 15', '150 x 90 x 10', '150 x 90 x 12', '150 x 90 x 15', '200 x 100 x 15', '200 x 150 x 15', '200 x 150 x 18' |
|---------------|--|



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2 Design Checks

| | |
|---------------|------|
| Design Status | Pass |
|---------------|------|

2.1 Selected Member Data

| | | | | |
|--|------------------------------|--------|--------------------------------|-------|
| | Section Size* | | ('75 x 75 x 5', 'Star Angles') | |
| | Material | | E 165 (Fe 290) | |
| | Mass, m (kg/m) | | 11.54 | |
| | Area, A (cm ²) | | 1472.0 | |
| | A (mm) | 75.0 | r_z (cm) | 3.1 |
| | B (mm) | 75.0 | r_y (cm) | 3.1 |
| | t (mm) | 5.0 | r_u (cm) | 3.25 |
| | T (mm) | 10.0 | r_v (cm) | 2.94 |
| | R_1 (mm) | 7.0 | Z_z (cm ³) | 18.83 |
| | R_2 (mm) | 0.0 | Z_y (cm ³) | 18.83 |
| | I_z (cm ⁴) | 141.26 | Z_{pz} (cm ³) | 30.03 |
| | I_y (cm ⁴) | 141.26 | Z_{py} (cm ³) | 30.03 |
| | I_u (cm ⁴) | 155.29 | Radius of gyration, r (cm) | 29.4 |
| | I_v (cm ⁴) | 127.23 | | |

2.2 Spacing Check

| Check | Required | Provided | Remarks |
|--------------------------|---|------------|---------|
| Min. Diameter (mm) | | $d = 16$ | |
| Hole Diameter (mm) | | $d_0 = 18$ | |
| Minimum Bolts (nos) | | $r_l = 1$ | |
| Min. Gauge Distance (mm) | $p/g_{\min} = 2.5d$ $= 2.5 \times 16.0$ $= 40.0$ [Ref. IS 800:2007, Cl.10.2.2] | 40 | Pass |



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| Check | Required | Provided | Remarks |
|-------------------------|---|----------|---------|
| Min. Edge Distance (mm) | $e_{\min} = 1.5d_0$ $= 1.5 \times 18.0$ $= 27.0$ <p>[Ref. IS 800:2007, Cl.10.2.4.2]</p> | 30 | Pass |
| Spacing Check | $\text{depth} = 2 e + (r_l - 1) g$ $= 2 \times 30 + (1 - 1) \times 40$ $= 60$ | 63.0 | Pass |

2.3 Member Check

| Check | Required | Provided | Remarks |
|--------------------------------|----------|--|---------|
| Tension Yielding Capacity (kN) | | $T_{dg} = \frac{A_g f_y}{\gamma_{m0}}$ $= \frac{1472.0 \times 165}{1.1 \times 10^3}$ $= 220.8$ <p>[Ref. IS 800:2007, Cl.6.2]</p> | |



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| Check | Required | Provided | Remarks |
|-------------------------------|----------|--|---------|
| Tension Rupture Capacity (kN) | | $\beta = 1.4 - 0.076 \times \frac{w}{t} \times \frac{f_y}{0.9f_u} \times \frac{b_s}{L_c}$ $\leq \frac{0.9f_u\gamma_{m0}}{f_y\gamma_{m1}} \geq 0.7$ $= 1.4 - 0.076 \times \frac{75.0}{5.0} \times \frac{165}{0.9 \times 290} \times \frac{113.5}{150}$ $\leq \frac{0.9 \times 290 \times 1.1}{165 \times 1.25} \geq 0.7$ $= 0.85$ $T_{dn} = 2 \times \left(\frac{0.9A_{nc}f_u}{\gamma_{m1}} + \frac{\beta A_{go}f_y}{\gamma_{m0}} \right)$ $= 2 \times \left(\frac{0.9 \times 260.0 \times 290}{1.25} + \frac{0.85 \times 375.0 \times 165}{1.1} \right)$ $= 204.2$ <p>[Ref. IS 800:2007, Cl.6.3.3]</p> | |
| Block Shear Capacity (kN) | | $T_{db1} = \frac{A_{vg}f_y}{\sqrt{3}\gamma_{m0}} + \frac{0.9A_{tn}f_u}{\gamma_{m1}}$ $T_{db2} = \frac{0.9A_{vn}f_u}{\sqrt{3}\gamma_{m1}} + \frac{A_{tg}f_y}{\gamma_{m0}}$ $T_{db} = \min(T_{db1}, T_{db2}) = 194.32$ <p>[Ref. IS 800:2007, Cl.6.4]</p> | |
| Tension Capacity (kN) | 180.0 | $T_d = \min(T_{dg}, T_{dn}, T_{db})$ $= \min(220.8, 204.2, 194.32)$ $= 194.32$ <p>[Ref. IS 800:2007, Cl.6.1]</p> | Pass |



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| Check | Required | Provided | Remarks |
|----------------------------|---|---|---------|
| Slenderness | $\frac{KL}{r} \leq 400$ | $\frac{KL}{r} = \frac{1 \times 2500.0}{29.4}$ $= 85.03$ [Ref. IS 800:2007, Cl.7.1.2] | Pass |
| Utilization Ratio | ≤ 1 | Utilization Ratio = $\frac{F}{T_d} = \frac{180.0}{194.32}$ $= 0.93$ | |
| Axial Load Considered (kN) | $A_{cmin} = 0.3A_c$ $= 0.3 \times 220.8$ $= 66.24$ $A_{cmax} = 220.8$ [Ref. IS 800:2007, Cl.10.7] | $A_u = 180.0$ | Pass |

2.4 Bolt Design

| Check | Required | Provided | Remarks |
|---|--|--|---------|
| Diameter (mm) | Bolt Quantity Optimization | $d = 16$ | |
| Hole Diameter (mm) | | $d_0 = 18$ | |
| Property Class | Bolt Grade Optimization | 5.6 | |
| Bolt Ultimate Strength (N/mm ²) | | $f_{ub} = 500.0$ | |
| Bolt Yield Strength (N/mm ²) | | $f_{yb} = 300.0$ | |
| Nominal Stress Area (mm ²) | | $A_{nb} = 157$ ([Ref. IS 1367 – 3 (2002)]) | |
| Min. Pitch Distance (mm) | $p_{min} = 2.5d$ $= 2.5 \times 16.0$ $= 40.0$ [Ref. IS 800:2007, Cl.10.2.2] | 50 | Pass |



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| Check | Required | Provided | Remarks |
|--------------------------|---|----------|---------|
| Max. Pitch Distance (mm) | $p/g_{\max} = \min(32t, 300)$ $= \min(32 \times 5.0, 300)$ $= \min(160.0, 300)$ $= 160.0$ <p>Where, $t = \min(10.0, 5.0)$</p> <p>[Ref. IS 800:2007, Cl.10.2.3]</p> | 50 | Pass |
| Min. Gauge Distance (mm) | $p_{\min} = 2.5d$ $= 2.5 \times 16.0$ $= 40.0$ <p>[Ref. IS 800:2007, Cl.10.2.2]</p> | 0 | |
| Max. Gauge Distance (mm) | $p/g_{\max} = \min(32t, 300)$ $= \min(32 \times 5.0, 300)$ $= \min(160.0, 300)$ $= 160.0$ <p>Where, $t = \min(10.0, 5.0)$</p> <p>[Ref. IS 800:2007, Cl.10.2.3]</p> | 0 | |
| Min. End Distance (mm) | $e_{\min} = 1.7d_0$ $= 1.7 \times 18.0$ $= 30.6$ <p>[Ref. IS 800:2007, Cl.10.2.4.2]</p> | 35 | Pass |



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| Check | Required | Provided | Remarks |
|-------------------------|---|--|---------|
| Max. End Distance (mm) | $e_{\max} = 12t\epsilon; \epsilon = \sqrt{\frac{250}{f_y}}$ $e_1 = 12 \times 5.0 \times \sqrt{\frac{250}{165}} = 73.85$ $e_2 = 12 \times 10.0 \times \sqrt{\frac{250}{250}} = 120.0$ $e_{\max} = \min(e_1, e_2) = 73.85$ <p>[Ref. IS 800:2007, Cl.10.2.4.3]</p> | 35 | Pass |
| Min. Edge Distance (mm) | $e_{\min} = 1.5d_0$ $= 1.5 \times 18.0$ $= 27.0$ <p>[Ref. IS 800:2007, Cl.10.2.4.2]</p> | 31.5 | Pass |
| Max. Edge Distance (mm) | $e_{\max} = 12t\epsilon; \epsilon = \sqrt{\frac{250}{f_y}}$ $e_1 = 12 \times 5.0 \times \sqrt{\frac{250}{165}} = 73.85$ $e_2 = 12 \times 10.0 \times \sqrt{\frac{250}{250}} = 120.0$ $e_{\max} = \min(e_1, e_2) = 73.85$ <p>[Ref. IS 800:2007, Cl.10.2.4.3]</p> | 31.5 | Pass |
| Kb | | $k_b = \min \left(\frac{e}{3d_0}, \frac{p}{3d_0} - 0.25, \frac{f_{ub}}{f_u}, 1.0 \right)$ $= \min \left(\frac{35}{3 \times 18.0}, \frac{50}{3 \times 18.0} - 0.25, \frac{500.0}{290}, 1.0 \right)$ $= \min(0.65, 0.68, 1.72, 1.0)$ $= 0.65$ <p>[Ref. IS 800:2007, Cl.10.3.4]</p> | |



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| Check | Required | Provided | Remarks |
|-----------------------|--|--|---------|
| Shear Capacity (kN) | | $V_{dsb} = \frac{f_{ub} n_n A_{nb}}{\sqrt{3} \gamma_{mb}}$ $= \frac{500.0 \times 1 \times 157}{1000 \times \sqrt{3} \times 1.25}$ $= 36.26$ <p>[Ref. IS 800:2007, Cl.10.3.3]</p> | |
| Bearing Capacity (kN) | | $V_{dpb} = \frac{2.5 k_b d t f_u}{\gamma_{mb}}$ $= \frac{2.5 \times 0.65 \times 16.0 \times 5.0 \times 290}{1000 \times 1.25}$ $= 30.16$ <p>[Ref. IS 800:2007, Cl.10.3.4]</p> | |
| Capacity (kN) | | $V_{db} = \min (V_{dsb}, V_{dpb})$ $= \min (36.26, 30.16)$ $= 30.16$ <p>[Ref. IS 800:2007, Cl.10.3.2]</p> | |
| No. of Bolts | $R_u = \sqrt{V_u^2 + A_u^2}$ $n_{trial} = R_u / V_{bolt}$ $R_u = \frac{\sqrt{0.0^2 + 180.0^2}}{30.16}$ $= 6$ | $n = 8$ | |
| No. of Bolt Columns | | $n_c = 4$ | |
| No. of Bolt Rows | | $n_r = 2$ | |



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| Check | Required | Provided | Remarks |
|------------------------------------|--|--|---------|
| Long Joint Reduction Factor | <p>if $l_j \geq 15d$ then $V_{rd} = \beta_{lj} V_{db}$</p> <p>if $l_j < 15d$ then $V_{rd} = V_{db}$</p> <p>where,</p> $l_j = ((n_c \text{ or } n_r) - 1) \times (p \text{ or } g)$ $\beta_{lj} = 1.075 - l/(200d)$ <p>but $0.75 \leq \beta_{lj} \leq 1.0$</p> <p>[Ref. IS 800:2007, Cl.10.3.3.1]</p> | $l_j = ((n_c \text{ or } n_r) - 1) \times (p \text{ or } g)$ $= (4 - 1) \times 50 = 150$ $= (2 - 1) \times 0 = 0$ $l = 150$ $15 \times d = 15 \times 16.0 = 240.0$ <p>since, $l_j < 15 \times d$ then $\beta_{lj} = 1.0$</p> <p>[Ref. IS 800:2007, Cl.10.3.3.1]</p> | |
| Large Grip Length Reduction Factor | <p>if $l_g \geq 5d$, then $V_{rd} = \beta_{lg} V_{db}$</p> <p>if $l_g < 5d$ then $V_{rd} = V_{db}$</p> $l_g \leq 8d$ <p>where,</p> $l_g = \Sigma(t_{ep} + t_{member})$ $\beta_{lg} = 8d/(3d + l_g)$ <p>but $\beta_{lg} \leq \beta_{lj}$</p> <p>[Ref. IS 800:2007, Cl.10.3.3.2]</p> | $l_g = \Sigma(t_p + t_{member})$ $= 15.0$ $5d = 80.0$ $8d = 128.0$ <p>since, $l_g < 5d$; $\beta_{lg} = 1.0$</p> <p>[Ref. IS 800:2007, Cl.10.3.3.2]</p> | |
| Capacity (kN) | 22.5 | $V_{rd} = \beta_{lj} \beta_{lg} V_{db}$ $= 1.0 \times 1.0 \times 30.16$ $= 30.16$ | Pass |



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2.5 Gusset Plate Check

| Check | Required | Provided | Remarks |
|--------------------------------|----------|--|---------|
| Min.Height (mm) | | $H = 2 \times \text{Depth} + \text{Clearance}$ $= (2 \times 75.0) + 30.0$ $= 180$ | |
| Min.Plate Length (mm) | | $L = (nc - 1)p + 2e$ $= (4 - 1) \times 50 + (2 \times 35)$ $= 220$ | |
| Min.Member Length (mm) | 440 | 2500.0 | Pass |
| Thickness (mm) | | $T = 10.0$ | |
| Tension Yielding Capacity (kN) | | $T_{dg} = \frac{A_g f_y}{\gamma_{m0}}$ $A_g = lt = 150.0 \times 10.0$ $= \frac{1500.0 \times 250}{1.1 \times 10^3}$ $= 340.91$ [Ref. IS 800:2007, Cl.6.2] | |
| Tension Rupture Capacity (kN) | | $T_{dn} = \frac{0.9 A_n f_u}{\gamma_{m1}}$ $= \frac{1 \times 0.9 \times (150.0 - 2 \times 18.0) \times 10.0 \times 410}{1.25}$ $= 336.53$ [Ref. IS 800:2007, Cl.6.3.1] | |
| Block Shear Capacity (kN) | | $T_{dbl1} = \frac{A_{vg} f_y}{\sqrt{3} \gamma_{m0}} + \frac{0.9 A_{tn} f_u}{\gamma_{m1}}$ $T_{dbl2} = \frac{0.9 A_{vn} f_u}{\sqrt{3} \gamma_{m1}} + \frac{A_{tg} f_y}{\gamma_{m0}}$ $T_{db} = \min(T_{db1}, T_{db2}) = 477.25$ [Ref. IS 800:2007, Cl.6.4] | |



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| Tension Capacity (kN) | $A = 180.0$ | $T_d = \min(T_{dg}, T_{dn}, T_{db})$ $= \min(340.91, 336.53, 477.25)$ $= 336.53$ [Ref.IS 800:2007, Cl.6.1] | Pass |

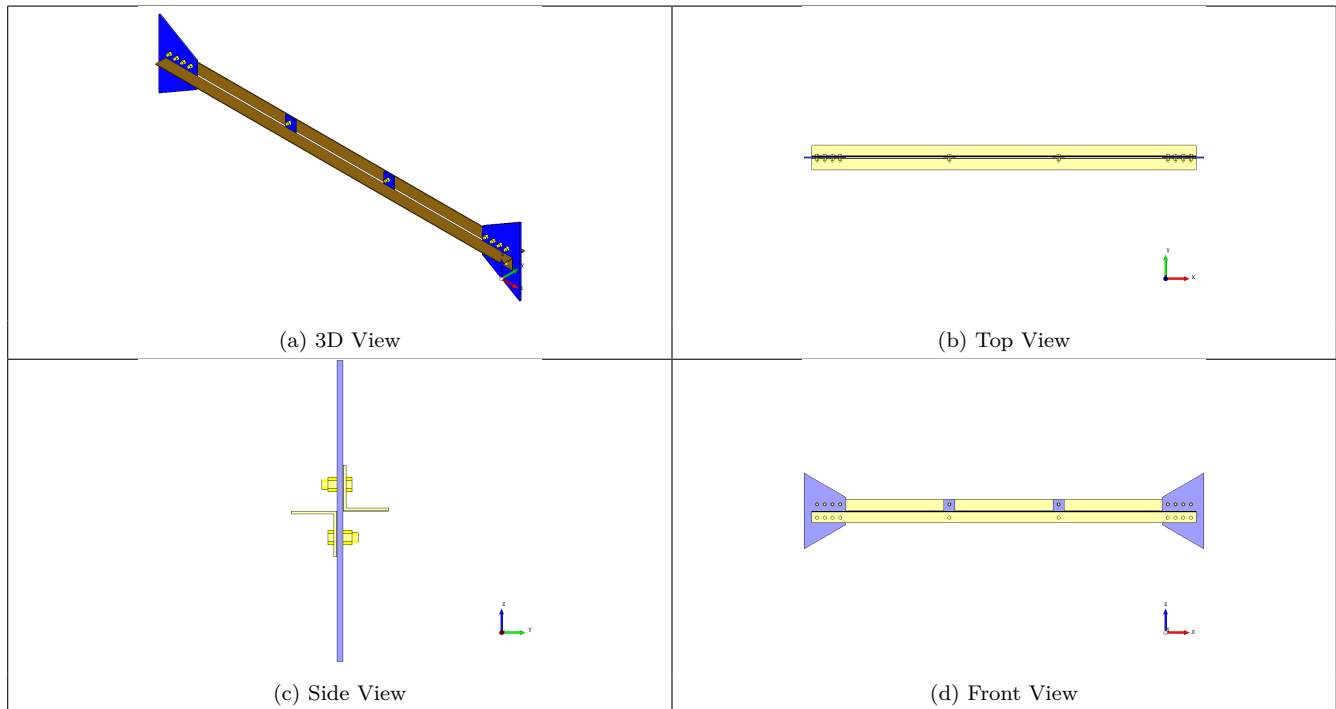
2.6 Intermittent Connection

| Check | Required | Provided | Remarks |
|-----------------------|----------|----------|---------|
| Connection (nos) | | 2 | |
| Spacing (mm) | 1000 | 710.0 | Pass |
| Diameter (mm) | | 16 | |
| Property Class | | 5.6 | |
| No. of Bolt Columns | | 1 | |
| No. of Bolt Rows | | 2 | |
| Min.Height (mm) | | 150 | |
| Min.Plate Length (mm) | | 70 | |



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3 3D Views



4 Design Log

2021-02-04 15:31:47 - Osdag - INFO - :In the case of reverse loading, the slenderness value shall be less than 180 [Ref. Table 3, IS 800:2007].

2021-02-04 15:31:47 - Osdag - INFO - :In the case of reverse loading for double sections, spacing of the intermittent connection shall be less than 600 [Ref. Cl. 10.2.5.5, IS 800:2007].

2021-02-04 15:31:47 - Osdag - INFO - :To reduce the quantity of bolts, define a list of diameter, plate thickness and/or member size higher than the one currently defined.

2021-02-04 15:31:47 - Osdag - INFO - :Overall bolted tension member design is safe.

2021-02-04 15:31:47 - Osdag - INFO - :=====End Of design=====